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2½D Finite Element Method for Electrical Impedance Tomography Considering the Complete Electrode Model

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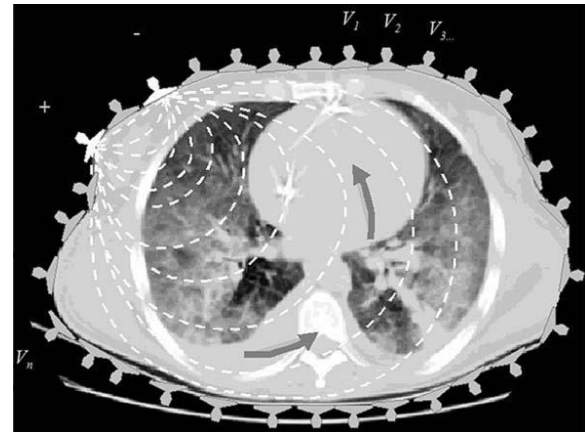
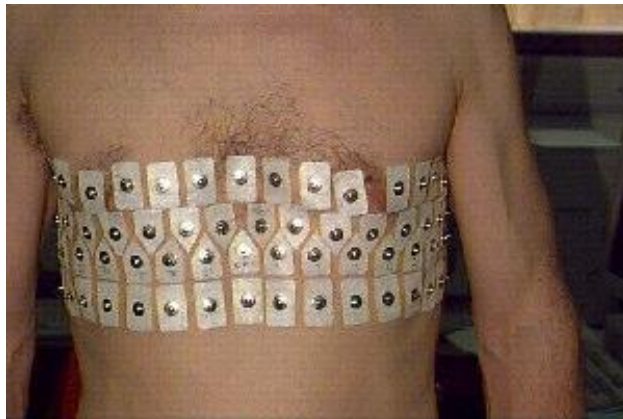
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Carleton University

Jan 2012

Electrical Impedance Tomography (EIT)

- EIT is used to generate images of the internal structure of sections of a body
- The EIT problem is
 - to reconstruct an unknown impedance distribution from boundary measurements.



Photos: (left) from Wikipedia/EIT, (right) from [4]

The EIT Problem

- Forward Model (2D & 3D)

$$\nabla_{2D} \cdot (\sigma(x,y) \nabla_{2D} \varphi(x,y)) = 0$$

$$\nabla_{3D} \cdot (\sigma(x,y,z) \nabla_{3D} \varphi(x,y,z)) = 0$$

$$\sigma \frac{\partial \phi}{\partial n} = \begin{cases} J & \text{on current electrodes} \\ 0 & \text{elsewhere on the surface} \end{cases}$$

- Finite Element Method
- Current Patterns
- Electrode Models

2½D Motivation

- The 3D FE Model recruits too much elements.
 - => requires much more memory and **Computational Complexity** vs. 2D
 - Both Forward and Inverse Problem
 - Specially the inverse part
 - Requires more calculation time
 - ≠ Real time
 - Or a super-computer for fast imaging
 - ≠ Portability and Inexpensiveness

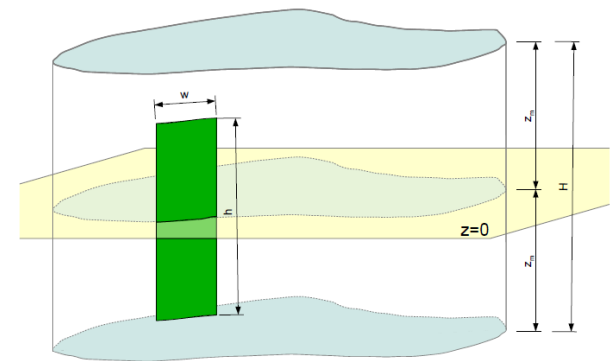
The 2½D Model

- Assumption
 - Translational Invariance along z
 - => Symmetric Voltages
- Equations

$$\nabla_{3D} \cdot (\sigma(x, y, z) \nabla_{3D} \varphi(x, y, z)) = 0$$

$$\varphi(x, y, z) = \sum_{k=0}^{\infty} V_k(x, y) \cos\left(\frac{k\pi}{a} z\right)$$

$$\begin{cases} \nabla_{2D} \cdot (\sigma(x, y) \nabla V_k(x, y)) - \sigma(x, y) \left(\frac{k\pi}{a}\right)^2 V_k(x, y) = 0 \\ \sigma(x, y) \frac{\partial}{\partial n} V_k(x, y) = J_k \end{cases}$$

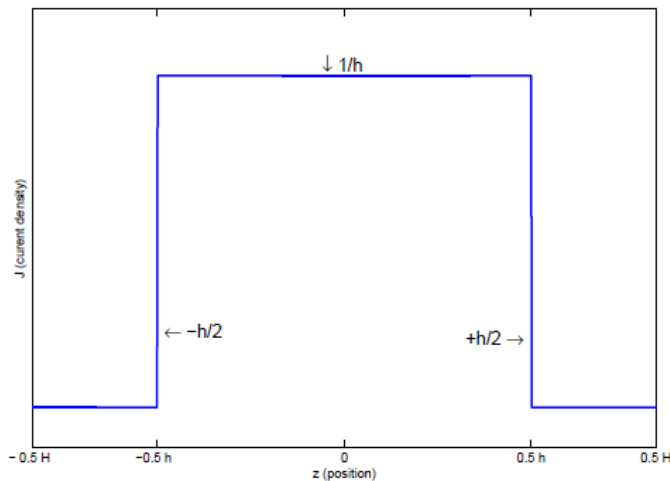


Boundary Condition $\sigma(x, y) \frac{\partial V_k}{\partial n} = J_k$

- for $I = 1$

$$J_0 = \frac{1}{H} = \frac{1}{2a}$$

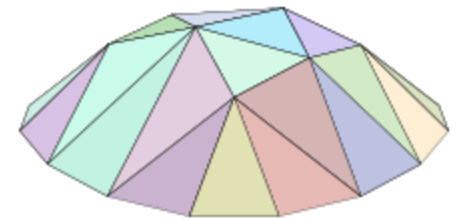
$$J_k = \frac{2}{k\pi h} \sin\left(\frac{k\pi h}{2a}\right)$$



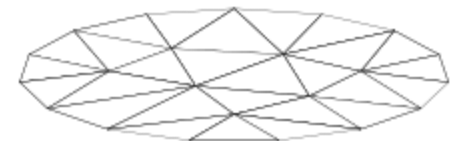
Finite Element Method

- Interpolation functions, i.e. basis

$$\tilde{u}_n(\vec{x}) = \sum_{i=1}^M u_i^n \phi_i(\vec{x})$$



- The Modified '*Stiffness Matrix*'



$$S'_{ij}{}^k = S_{ij}{}^k + \left(\frac{n\pi}{a}\right)^2 R_{ij}{}^k = \int_{E_k} \nabla\phi_i \cdot \nabla\phi_j + \left(\frac{n\pi}{a}\right)^2 \phi_i\phi_j d\Omega$$

$$S'(n)U_n = I_n$$

Inverse Problem of EIT

- Static EIT, Difference EIT
- Jacobian (Sensitivity Matrix)

$$z = \Delta v = v_{\sigma_2} - v_{\sigma_1}$$

$$x = \mathbf{J}z + n$$

$$x = \Delta \sigma = \sigma_2 - \sigma_1$$

$$\mathbf{J} = T \left[-\frac{\partial}{\partial \sigma} S^{-1}(\sigma) I \right] = T \left[S^{-1}(\sigma) \frac{\partial}{\partial \sigma} S(\sigma) S^{-1}(\sigma) I \right]$$

$$\hat{x} = (\mathbf{J}^T \mathbf{J})^{-1} \mathbf{J}^T z$$

$$\hat{x} = (\mathbf{J}^T \mathbf{J} + \lambda^2 \mathbf{R}^T \mathbf{R})^{-1} \mathbf{J}^T z = Bz$$

Inverse Problem in 2½D

- Using Jacobian:

- For each $n \rightarrow \Delta v_n$

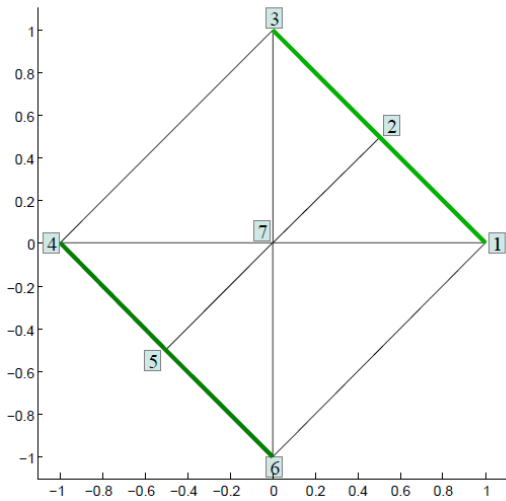
- $n \rightarrow S_n \rightarrow J_n \rightarrow \Delta\sigma_n$

$$\Delta v_n = J_n \Delta\sigma$$

$$J = \sum_{n=0}^{\infty} J_n$$

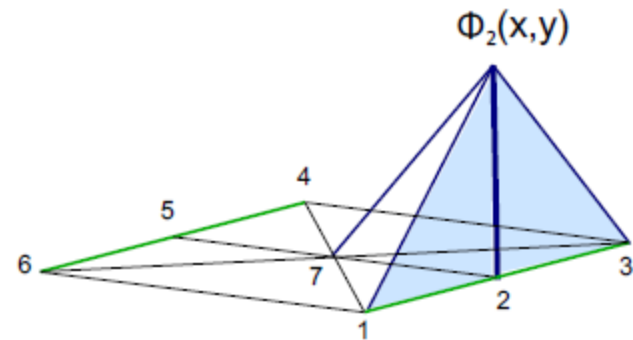
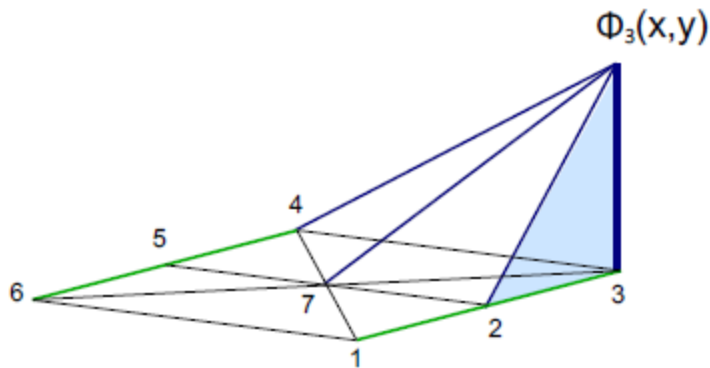
$$\Delta v = \sum_{k=0}^{\infty} \Delta v_k \cos\left(\frac{k\pi}{a} z\right)$$

Complete Electrode Model

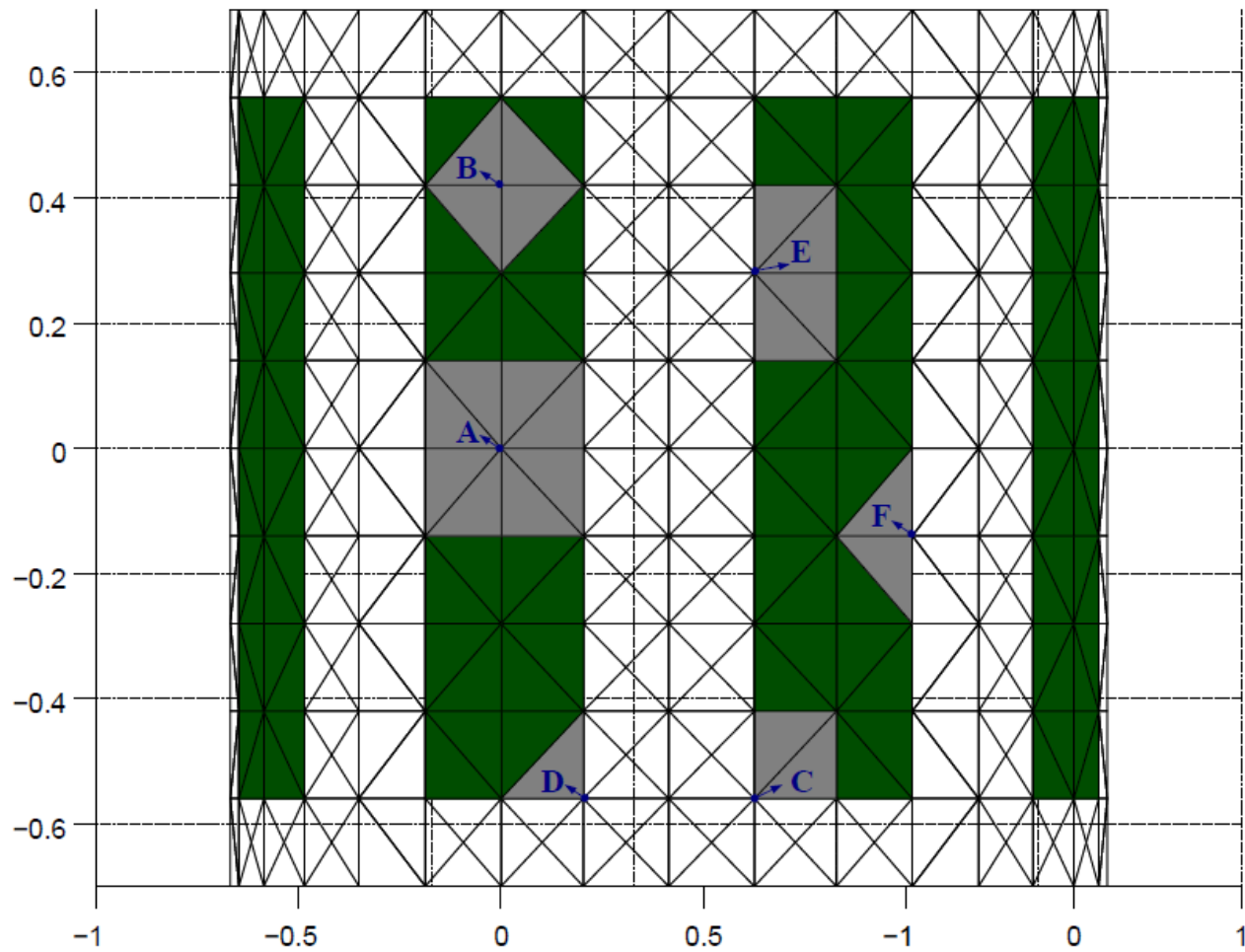


$$\begin{bmatrix} A_M + A_Z & A_W \\ A_W^T & A_D \end{bmatrix} \begin{bmatrix} U \\ V \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ I \end{bmatrix}$$

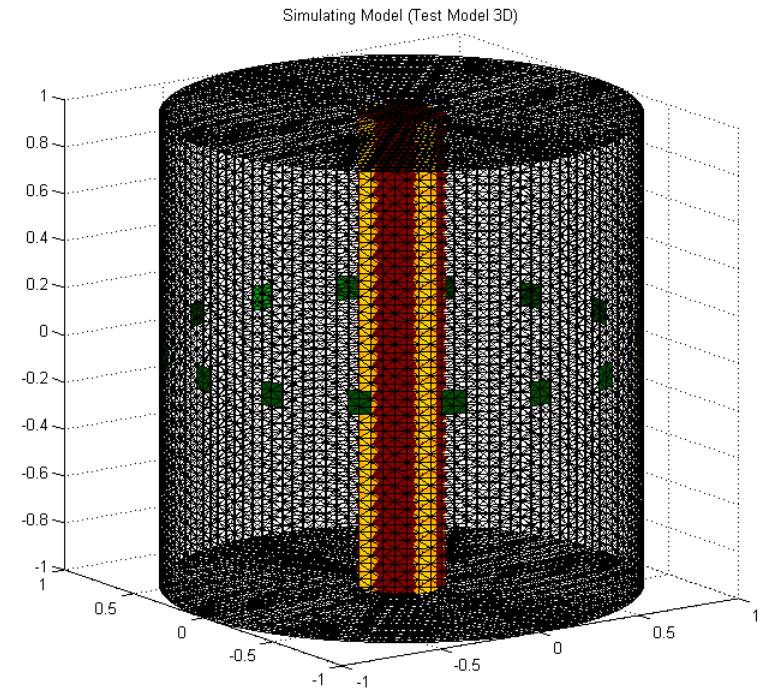
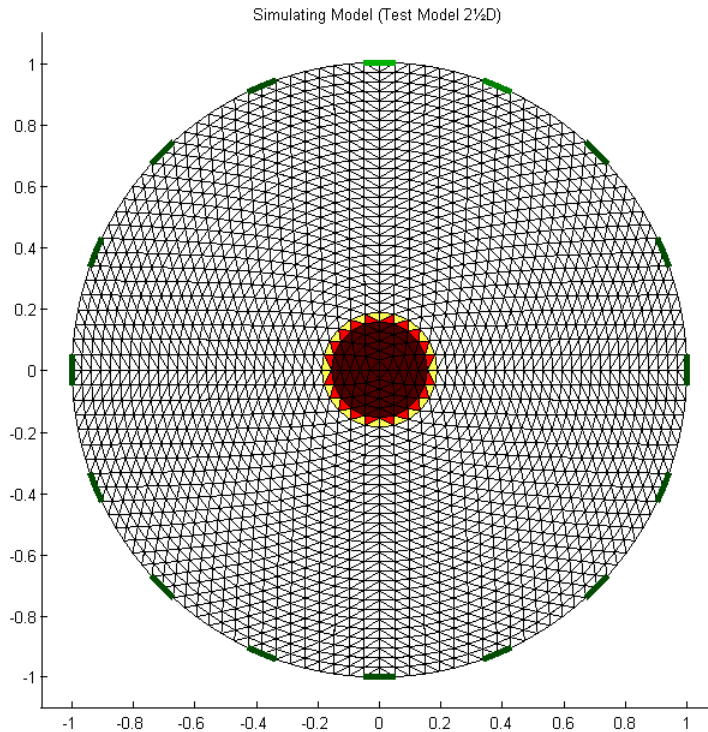
$$A_W = \begin{bmatrix} -\frac{\Delta}{2z_c} & -\frac{\Delta}{z_c} & -\frac{\Delta}{2z_c} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\frac{\Delta}{2z_c} & -\frac{\Delta}{z_c} & -\frac{\Delta}{2z_c} & 0 \end{bmatrix}^T$$



3D CEM



Mesh



2D mesh with 4096 elements used for the 2½D method (32 layers in xy)

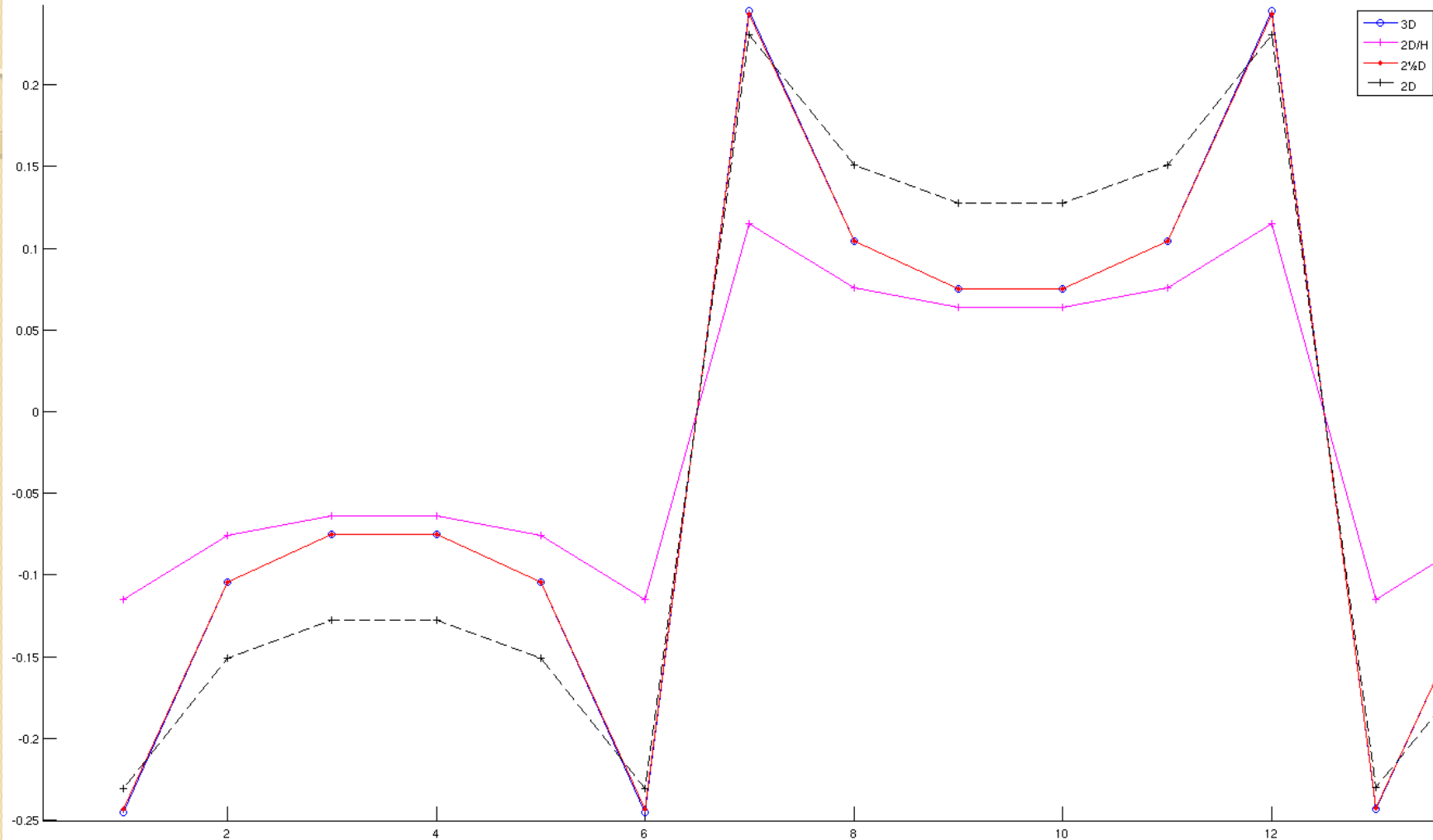
3D mesh with 737,280 elements (61 layers in z)

$H=2$; $h=0.1$, $w \approx 0.1$

The Images are produced by EIDORS

Results for Measurements

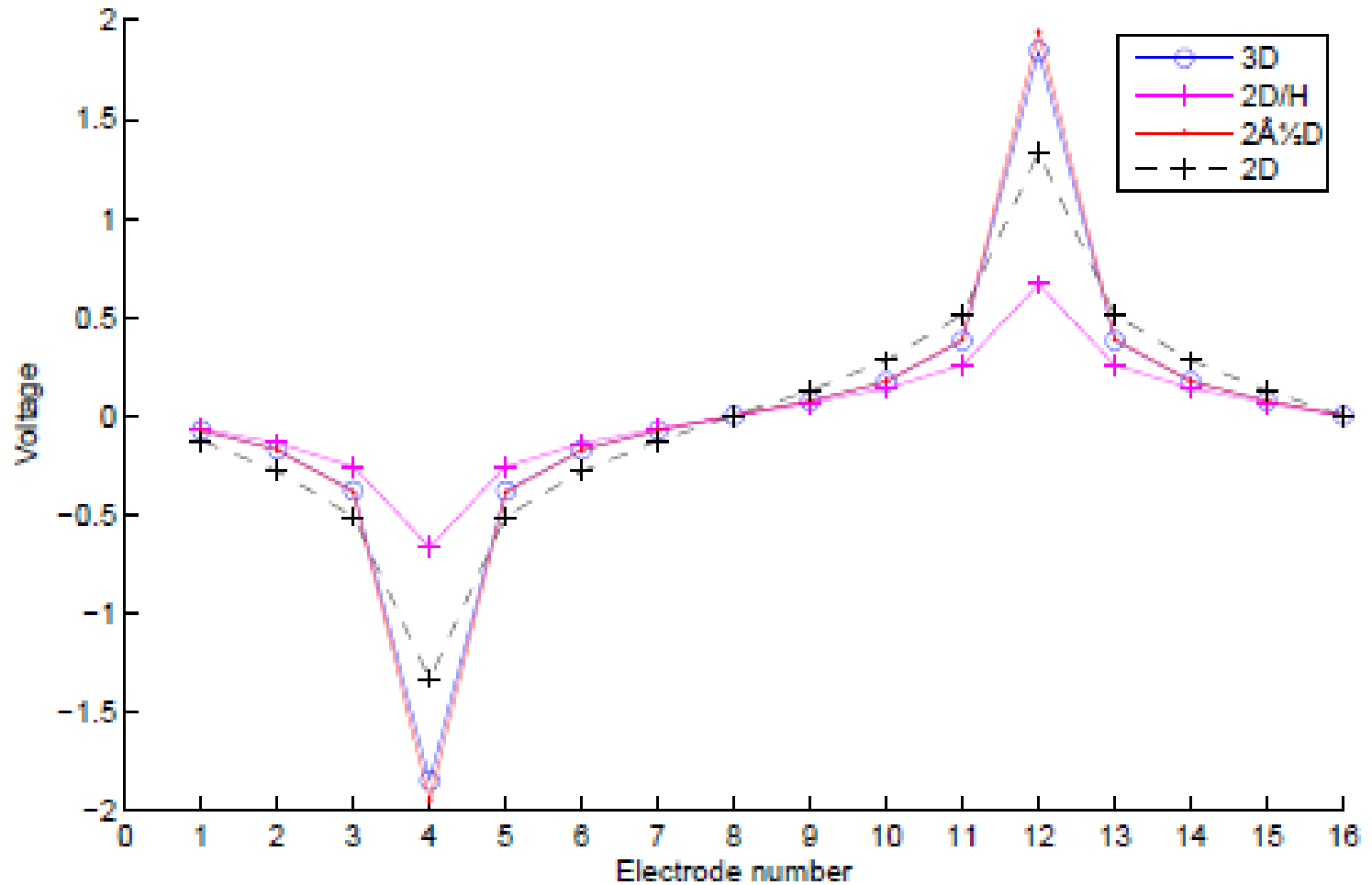
Tank height: 2, Object height: 2, Elect height: 0.1, Elect width: 0.098165, Domain height: 2, MAX_w: 4



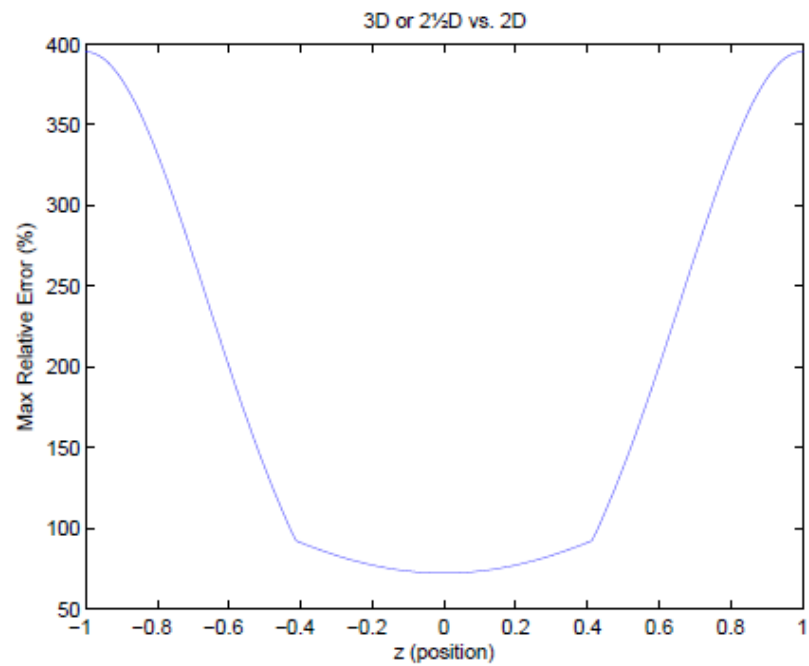
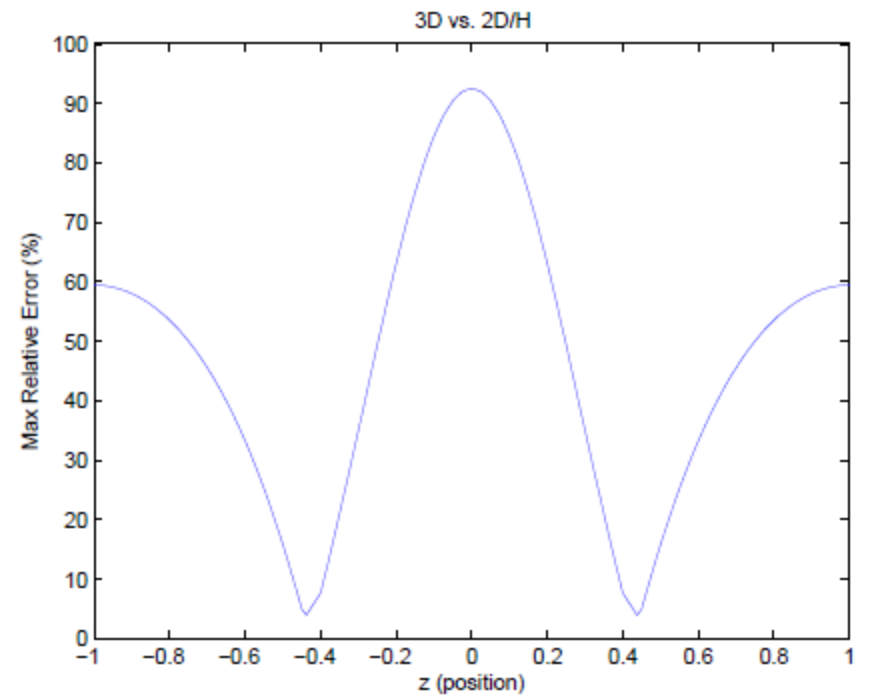
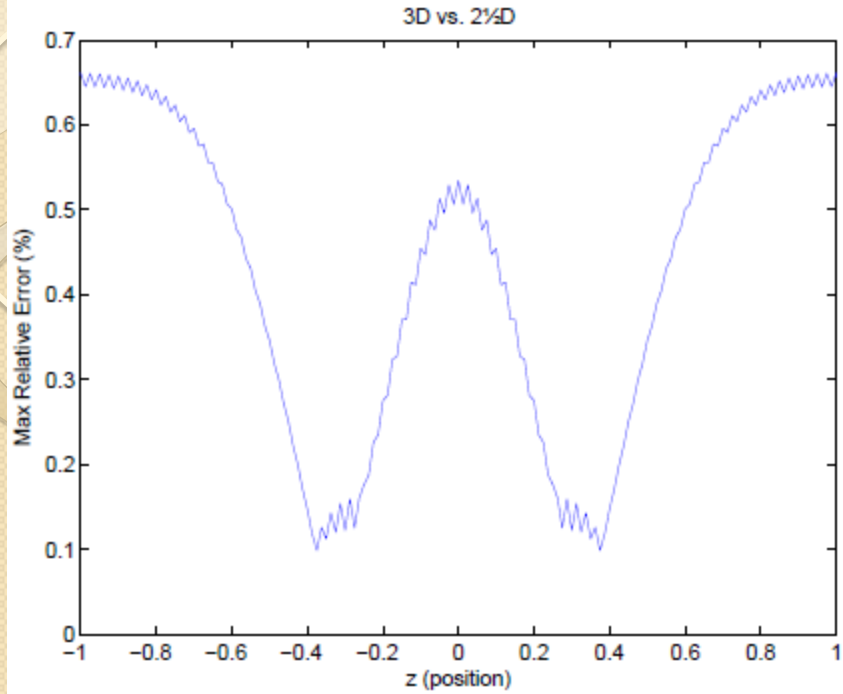
Measurements (Difference Voltage of Electrodes) – Opposite Pattern - Only first 5 terms

Maximum error: 0.82% (0.002)

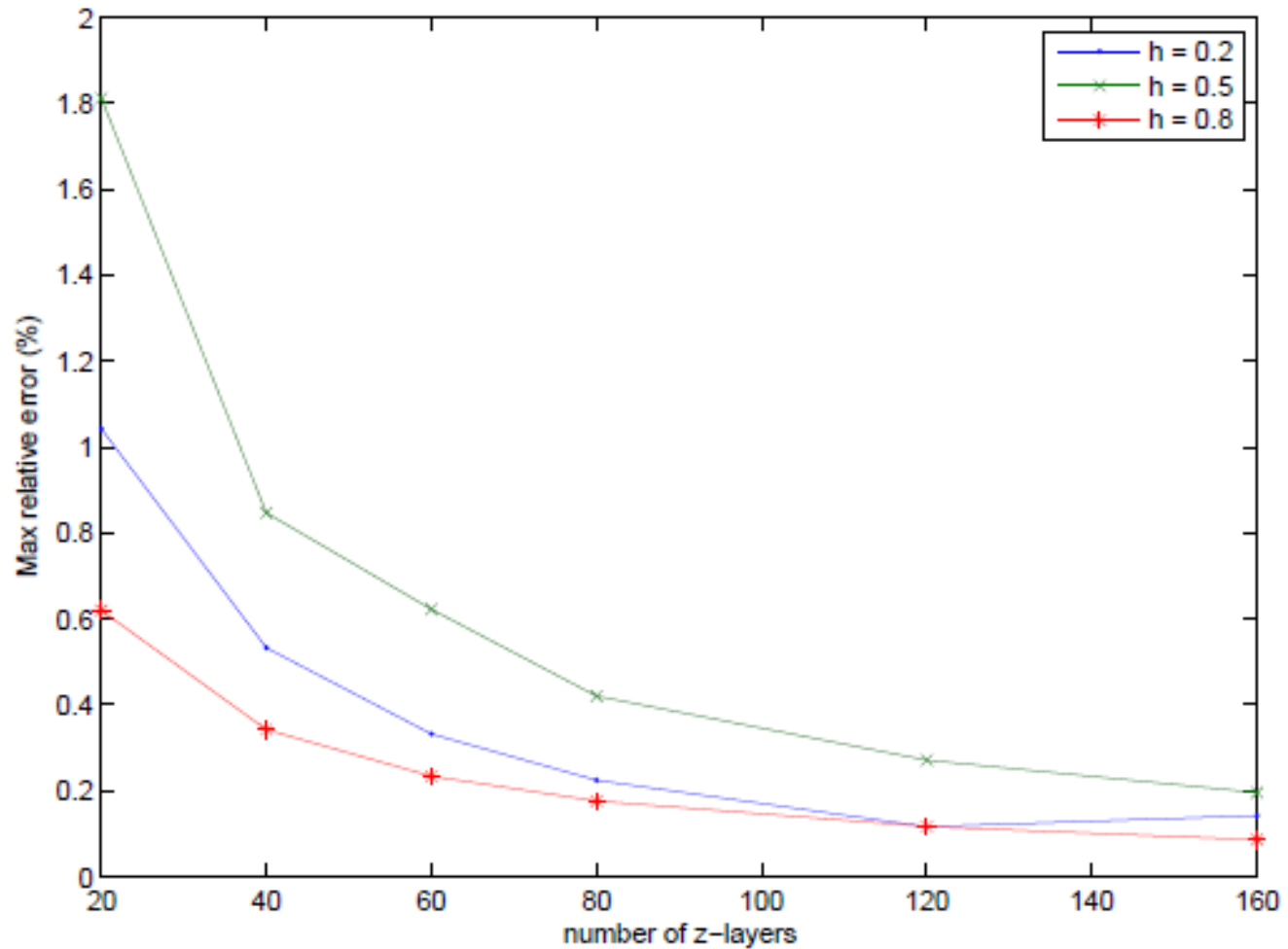
Tank height: 2, Object height: 2, Elect height: 0.4, Elect width: 0.098185, Domain height: 2, $MAX_N: 50$



Comparing 3D, 2D, 2D/H (first term of 2 1/2 D) and 2 1/2 D CEM solutions for electrode voltages - CEM ($W = 0.1, H = 2, h = 0.4$)

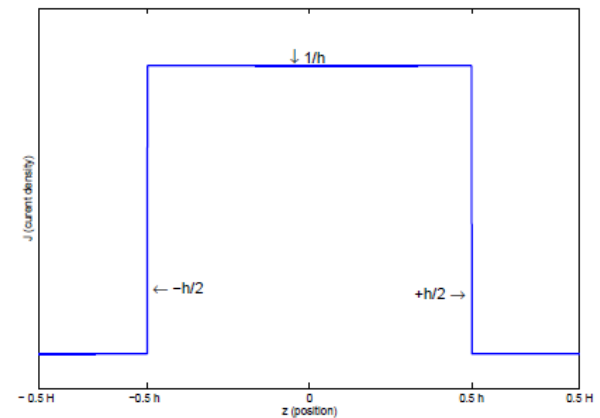
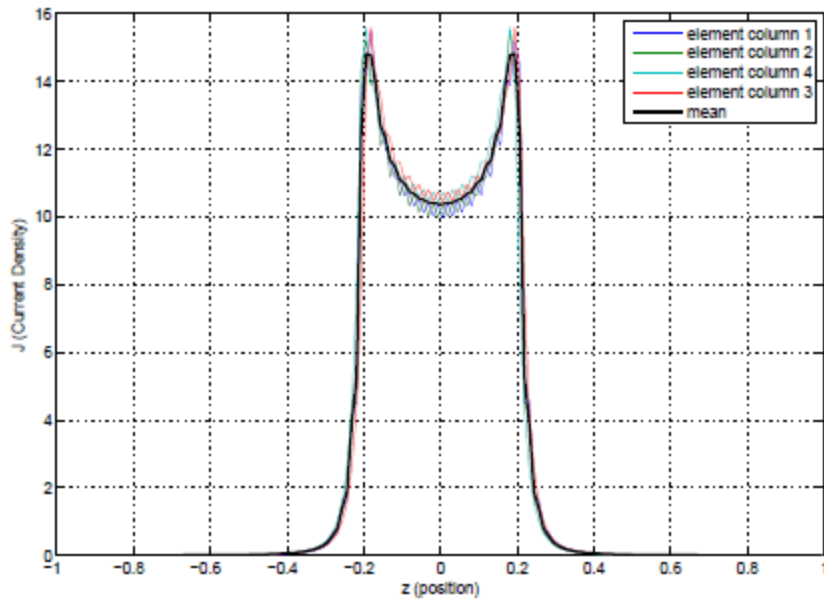


Decrement of the Error by Decrement of the Element size



Sources of Mismatch

- 3D Interpolation Function
- Injected Current Pattern

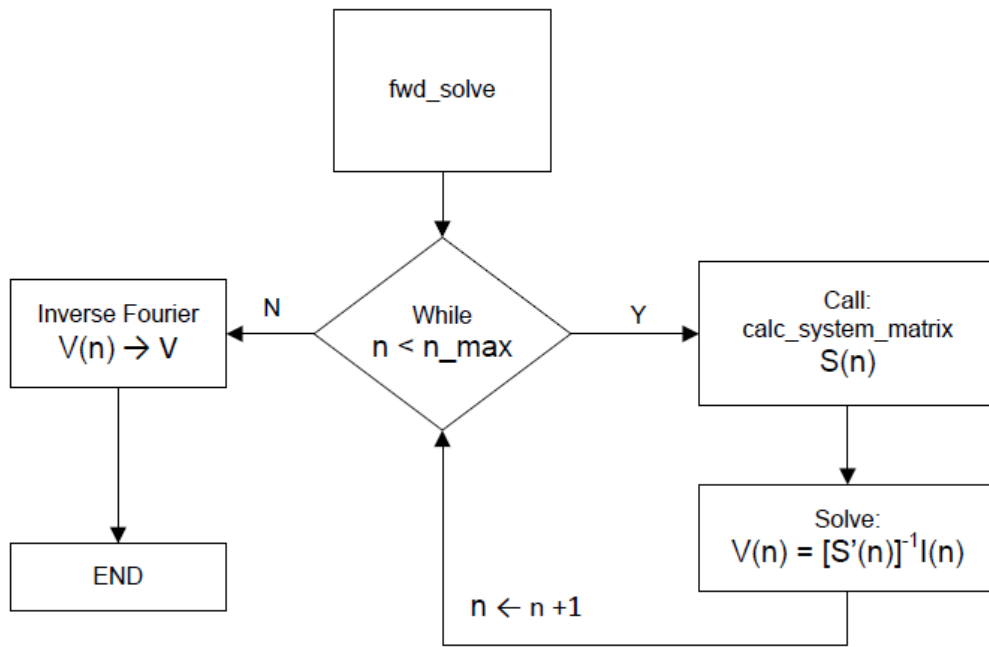


- 2D-based Complete Electrode Modelling

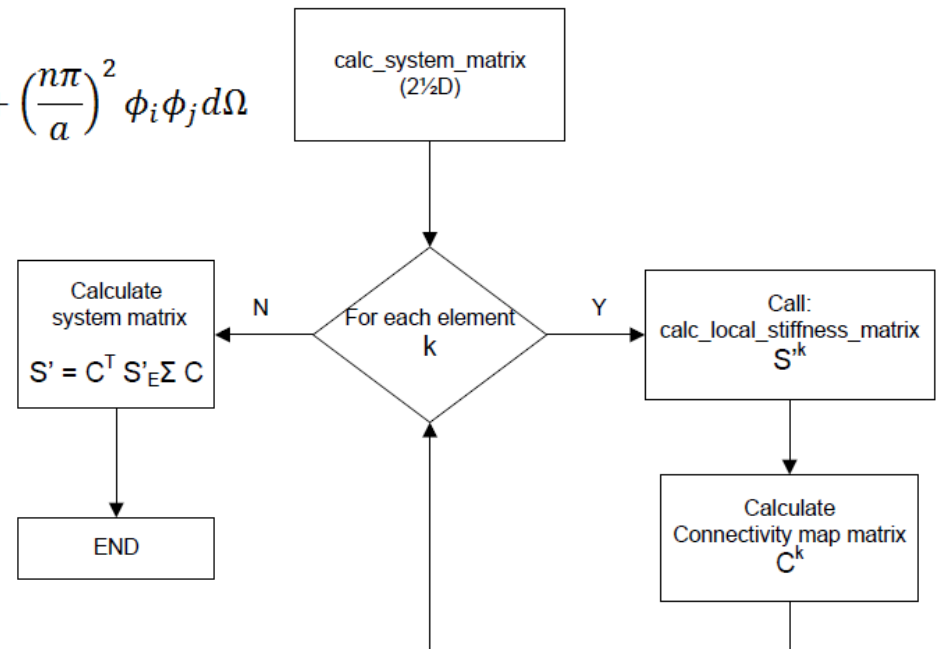
Truncation Point

$$V_{2\frac{1}{2}D} = \frac{1}{H}S^{-1}I + \sum_{n=1}^{\infty} \frac{2}{n\pi h} \sin\left(\frac{n\pi h}{2z_m}\right) \cos\left(\frac{n\pi}{z_m}z\right) \left(S + \left(\frac{n\pi}{z_m}\right)^2 R\right)^{-1} I$$

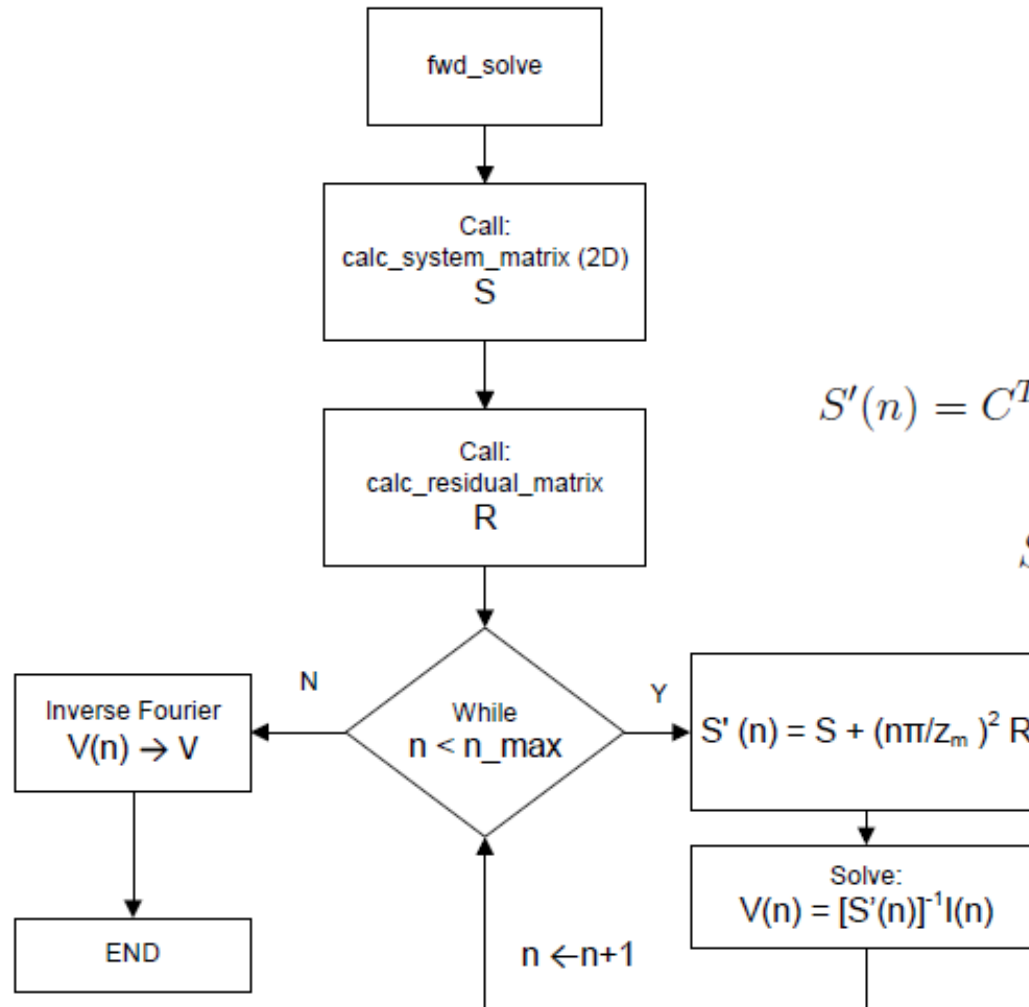
$\frac{H}{r}$	2		4		10	
	$\frac{h}{H}$	n_{max}	$\frac{h}{H}$	n_{max}	$\frac{h}{H}$	n_{max}
	(0.025, 0.05, 0.1)	3	(0.025)	7	(0.025)	13
	(> 0.1)	2	(0.05)	6	(0.05)	11
			(0.1)	5	(≥ 0.1)	7
			(≥ 0.2)	3		



$$S'_{ij}{}^k = S_{ij}^k + \left(\frac{n\pi}{a}\right)^2 R_{ij}^k = \int_{E_k} \nabla\phi_i \cdot \nabla\phi_j + \left(\frac{n\pi}{a}\right)^2 \phi_i\phi_j d\Omega$$



Speed/Computation Improvement



$$R = C^T R_E \Sigma C$$

$$R_{ij}^k = \int_{E_k} \phi_i \phi_j d\Omega$$

$$S'(n) = C^T S_E \Sigma C + \left(\frac{n\pi}{z_m}\right)^2 (C^T R_E \Sigma C)$$

$$S'(n) = S + \left(\frac{n\pi}{z_m}\right)^2 R$$

Achievements

$$t_{2\frac{1}{2}D} = t_{2D} + n_{max} \times t_{2D\text{-size Forward_Solve}} + t_R + t_{IFT}$$

Mesh Structure:

$$[2\frac{1}{2}D : Mesh.Nodes]_{N \times 2} \quad \text{vs.} \quad [3D : Mesh.Nodes]_{MN \times 3}$$

$$[2\frac{1}{2}D : Mesh.Elements]_{K \times 3} \quad \text{vs.} \quad [3D : Mesh.Nodes]_{3(M-1)K \times 4}$$

2D: 2,113 nodes and 4,094 elements

if M = 61 slices

3D: 128,893 nodes and 736,920 elements

System Matrix:

$$[S_{2\frac{1}{2}D}]_{N \times N} \quad \text{vs.} \quad [S_{3D}]_{MN \times MN}$$

$$M^2 = 61 \times 61 = 3,681$$

Matrix Inversion at the Forward Problem:

$$[S_{2\frac{1}{2}D}^{-1}]_{N \times N} \quad \text{vs.} \quad [S_{3D}^{-1}]_{MN \times MN}$$

$$M^2 = 61 \times 61 = 3,681$$

The EIDORS Project



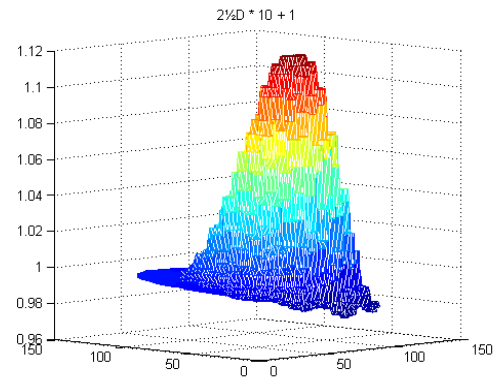
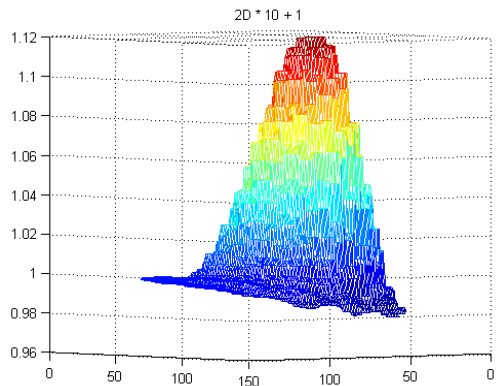
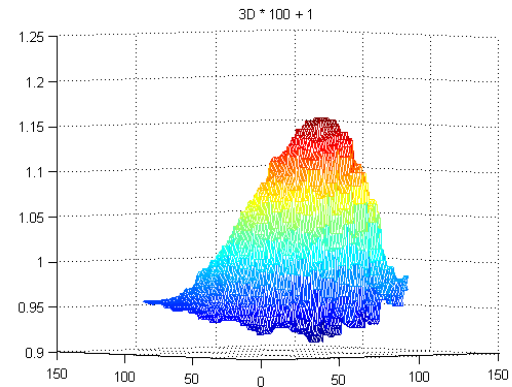
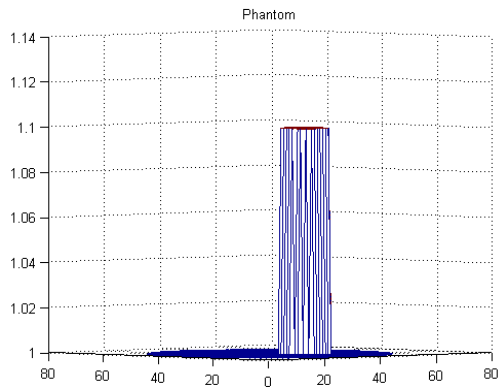
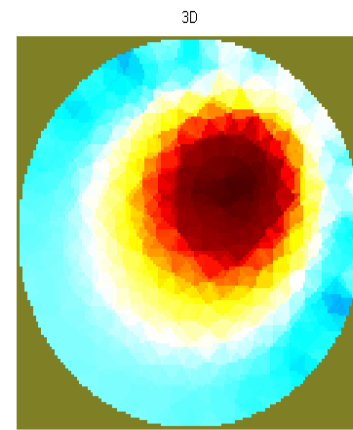
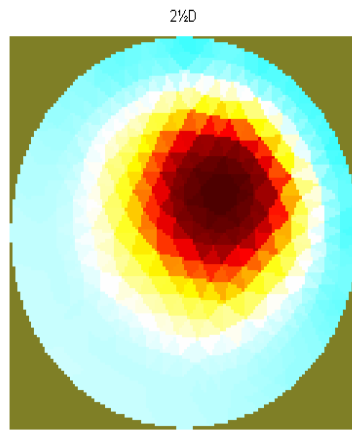
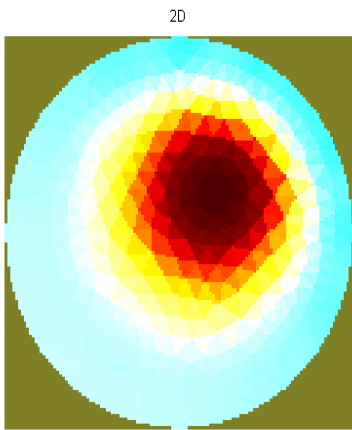
- <http://eidors3d.sourceforge.net/>
- ***Electrical Impedance and Diffuse Optical Tomography Reconstruction Software***
- A collaborative project where many groups working on EIT are involved around the world
- Modular-Based structure
- Medical & Industrial Applications

Questions

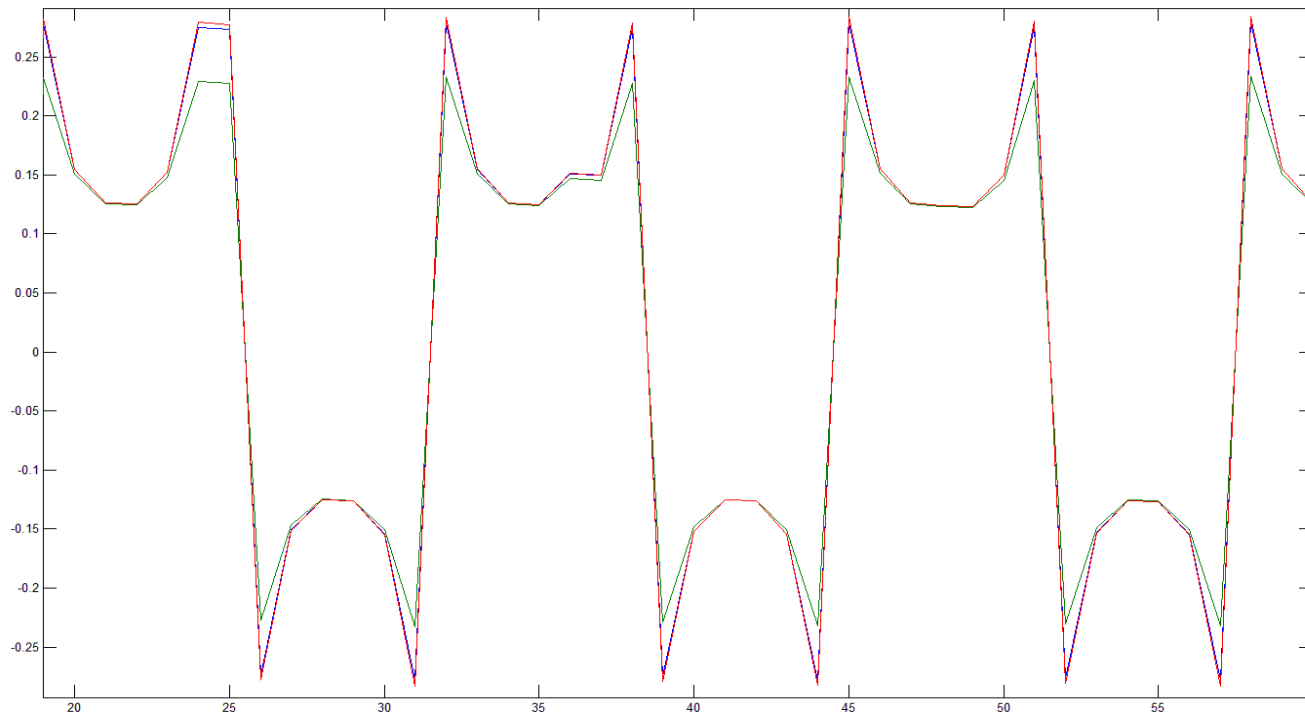
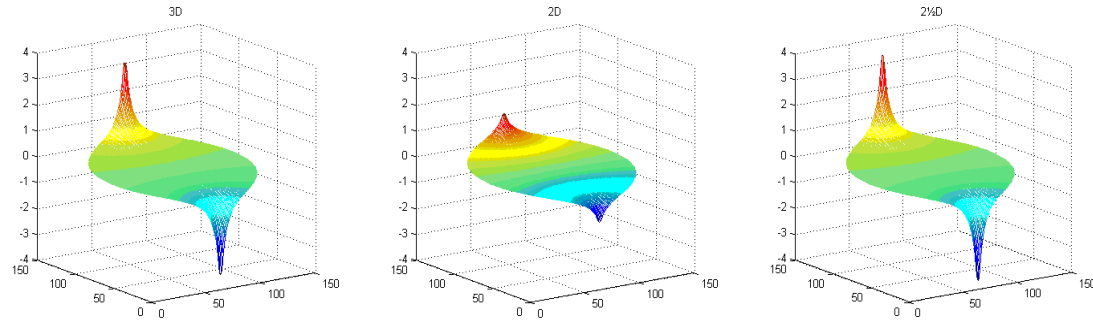
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Reference

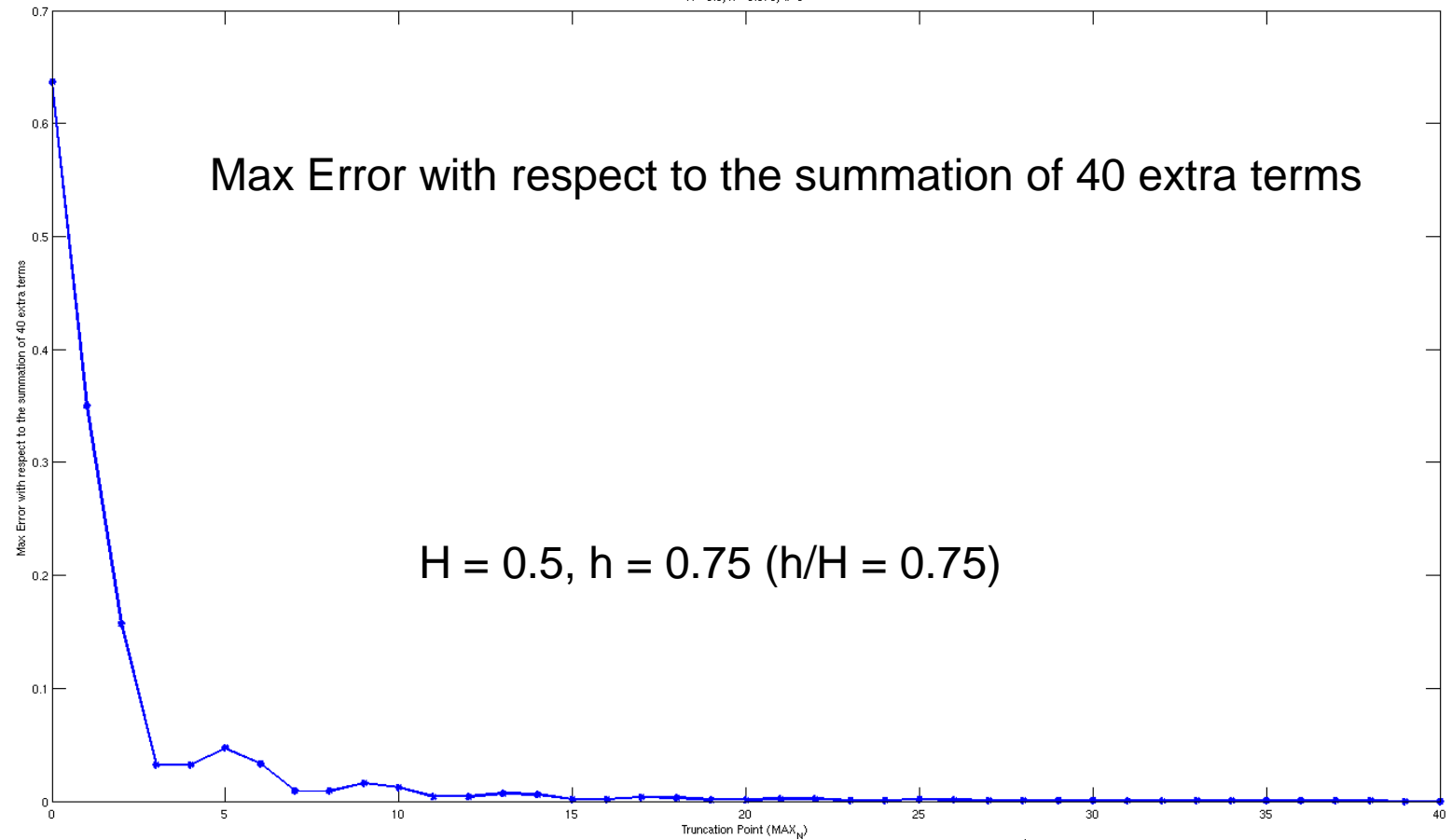
- [0] Ider *et al*, *Electrical impedance tomography of translationally uniform cylindrical objects with general cross-sectional boundaries*. *IEEE Trans. Med. Imaging* 9 49–59, 1990.
- [1] Lionheart W R B, *Uniqueness, shape and dimension in EIT*, *Ann. NY Acad. Sci.* 873 466–71, 1999
- [2] K Jerbi, W R B Lionheart, *et al* *sensitivity matrix and reconstruction algorithm for EIT assuming axial uniformity*, *Physiol. Meas.* 21 (2000) 61–66
- [3] David Holder, *Electrical impedance tomography: methods, history, and applications*, 2004
- [4] Costa E.L.V., Lima R. Gonzalez, Amato M.B.P., “*Electrical Impedance Tomography*”, *Yearbook of Intensive Care and Emergency Medicine*, 2009.
- [6] ...



Results of the Forward Model

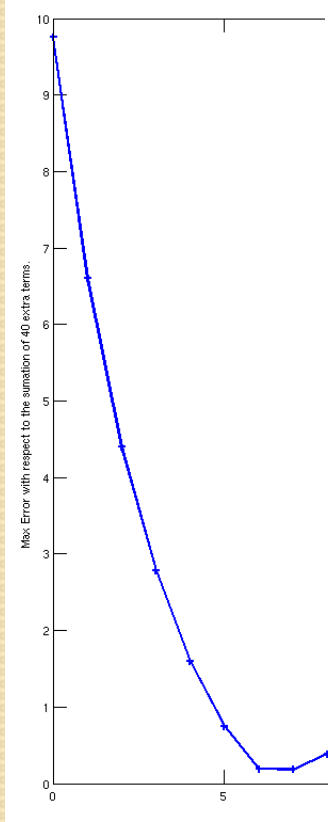


Max Error with respect to the summation of 40 extra terms



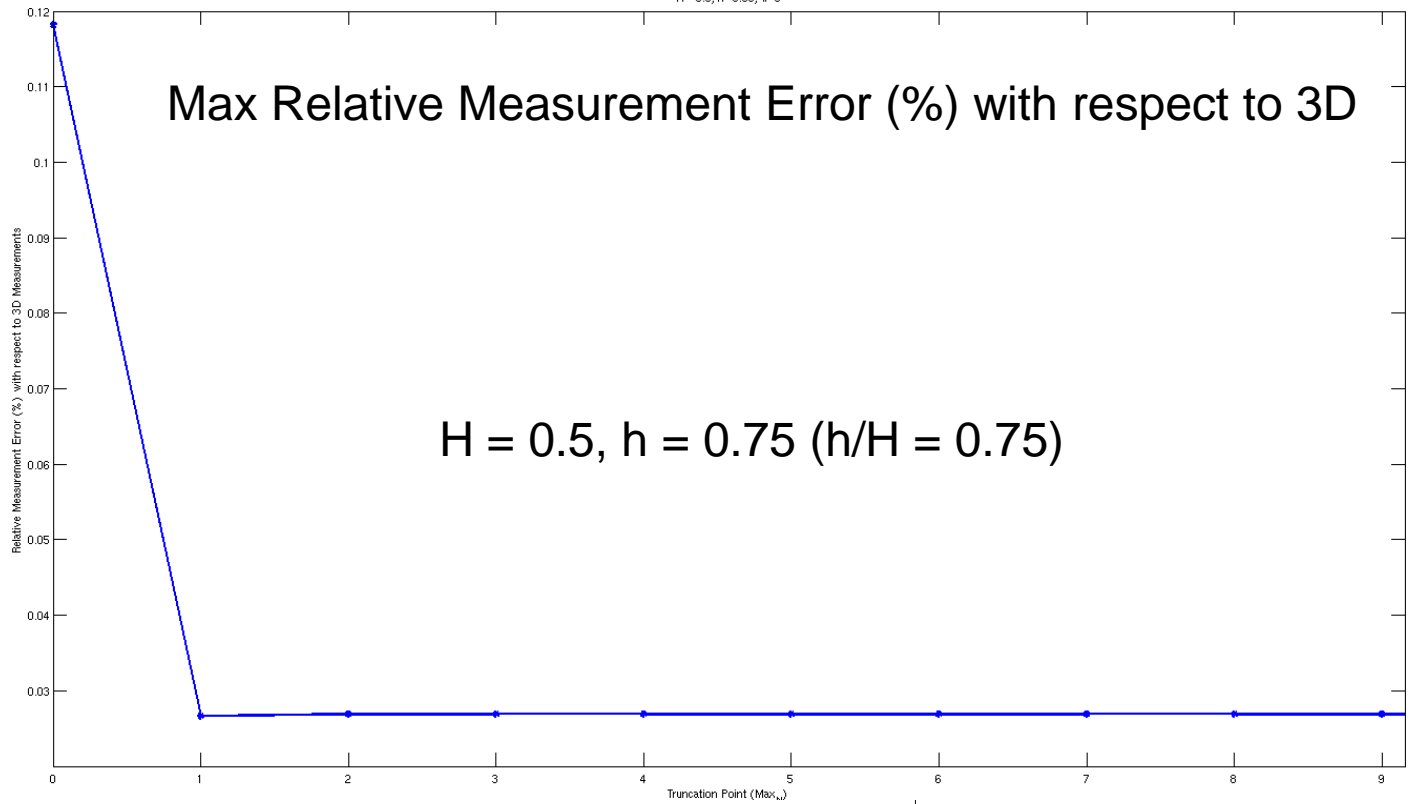
H = 0.5, h = 0.75 (h/H = 0.75)

H = 0.5, h = 0.05 (h/H = 0.1)

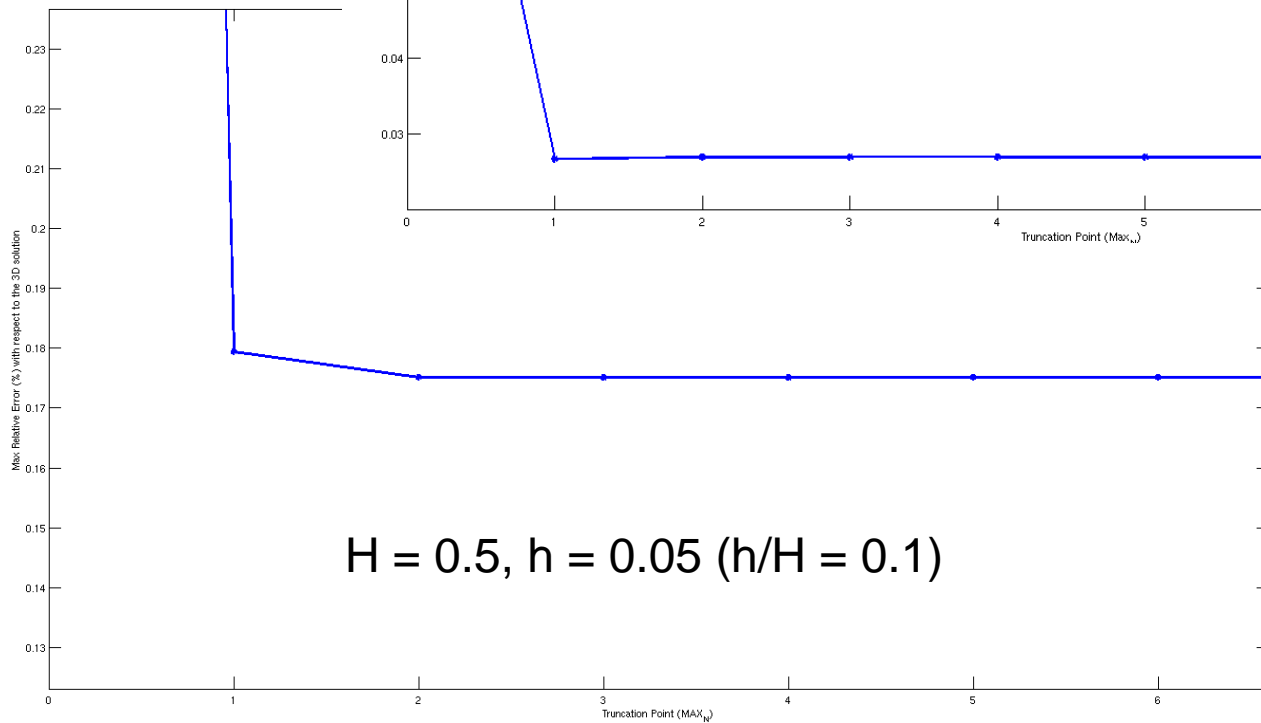


H = 0.5, h = 0.05, w = 0

Max Relative Measurement Error (%) with respect to 3D



H = 0.5, h = 0.75 (h/H = 0.75)



H = 0.5, h = 0.05 (h/H = 0.1)

Decrement of the Error by Decrement of the Element size

