The op-amp is ideal, with $V_{CC} = 10\, \text{V}$ and $V_{EE} = -10\, \text{V}$. The diode forward voltage, $V_D = 0.7\, \text{V}$.

This is a Wien bridge sine-wave oscillator. It oscillates because

$G = 1 + \frac{83\, \text{k}\Omega}{25\, \text{k}\Omega} = 4.32 > 3$.

- What is the frequency of oscillation.
- Sketch $V_o$ when the oscillation amplitude has stabilized.
- Indicate the approximate voltage of oscillation on the sketch.

$$\omega = (RC)^{-1} = (24\, \text{k}\Omega \times 24\, \text{nF})^{-1} = 1736.1 \, \text{rad/s}$$

$$f = \frac{1}{2\pi}\omega = 276.3\, \text{Hz}$$

- Sketch $V_o$ when the oscillation amplitude has stabilized.
  The oscillation will be roughly sine shaped at $f = 276.3\, \text{Hz}$
- Indicate the approximate voltage of oscillation on the sketch.
  amplitude stabilized at $\pm 0.7\, \text{V}$.
The op-amp is ideal, with $V_{CC} = 2\,V$ and $V_{EE} = -2\,V$.

![Circuit Diagram]

Initial conditions are: $V_- = 0$ and $V_o = +V_{CC}$.

Sketch as a function of time: 1) $V_-$, 2) $V_+$, 3) $V_o$

- $V_o$ will switch between $\pm 2\,V$
- $V_+$ will switch between $\pm 2\,V \cdot \frac{50\,k\Omega}{50\,k\Omega+38\,k\Omega} = 1.14\,V$
- $V_+$ will exponentially rise between $\pm 1.14\,V$.

Timing will be symmetric between +ve and -ve pulses.

$$(V_f - V_\infty) = (V_i - V_\infty)e^{-t/\tau},$$
where $\tau = RC = 24\,k\Omega \times 24\,nF = 0.576\,ms$

For the -ve transition, $V_i = 1.14\,V$, $V_f = -1.14\,V$, and $V_\infty = -2\,V$.

$$t = \tau \ln \left( \frac{V_f - V_\infty}{V_i - V_\infty} \right) = (0.576\,ms) \ln \left( \frac{1.14 - (-2)}{-1.14 - (-2)} \right) = 0.75\,ms$$
Initial conditions are that the charge on the capacitor is zero. $V_{CC} = 9\, \text{V}$.

- Sketch $V_o$, $V_A$ and $V_B$.
- What is the length of the $V_o = \text{high}$ and $V_o = \text{low}$ outputs?

This configuration is similar, but not the same as the configuration discussed in class. Normally $V_+$ of the upper comparator is connected to $V_B$. This means that the upper transitions will not happen at $V_B = \frac{2}{3}V_C C$, but instead when $V_A = \frac{2}{3}V_C C$. At this time, we calculate

$$i = (V_{CC} - \frac{2}{3}V_{CC})/36\, \text{k}\Omega = (9\, \text{V} - 6\, \text{V})/36\, \text{k}\Omega = 3\, \text{V}/36\, \text{k}\Omega = 83.33\, \mu\text{A}.$$ 

Using $i$, we calculate $V_B = V_A - i(17\, \text{k}\Omega) = 4.58\, \text{V}$.

Another way to see this is to think about Capacitor $C$ charging until $V_A = 2/3V_{CC}$ (RESET) and discharging until $V_B = 1/3V_{CC}$ (SET). In the usual 555 astable configuration, the trigger and threshold pins (pins 2 and 6) are both connected to the top of $C$, so $V_A = V_B$, however in the above circuit $V_A$ and $V_B$ are related by

$$V_A = V_B + (V_{CC} - V_B) \frac{R_B}{R_A + R_B}$$

(voltage divider). Setting $V_A = 2/3V_{CC}$ and rearranging, RESET occurs when $V_B$ reaches voltage $V_R$ given by

$$V_R = \left(\frac{2}{3} - \frac{R_B}{R_A + R_B}\right) \left(\frac{R_A + R_B}{R_A}\right) V_{CC}$$

$$V_R = \left(\frac{2}{3} - \frac{17\, \text{k}\Omega}{36\, \text{k}\Omega + 17\, \text{k}\Omega}\right) \left(\frac{36\, \text{k}\Omega + 17\, \text{k}\Omega}{36\, \text{k}\Omega}\right) 9\, \text{V} = 4.58\, \text{V}$$

The durations of the charge and discharge half-cycles are then given by the usual formula

$$t = RC \ln \left(\frac{V_\infty - V_i}{V_\infty - V_f}\right) = (0.31)RC$$
with $V_i = V_{CC}/3$, $V_f = V_R$, $V_\infty = V_{CC}$ and $R = R_A + R_B$ for the charge half-cycle and $V_i = V_R$, $V_f = V_{CC}/3$, $V_\infty = 0$ and $R = R_B$ for the discharge half-cycle. $V_o = V_{CC}$ during the charge period and $V_o = 0$ V during the discharge period. Thus:

- $t_{\text{high}} = 0.31 \times 51 \mu F \times (36 \, k\Omega + 17 \, k\Omega) = 0.84 \, ms$
- $t_{\text{low}} = 0.31 \times 51 \mu F \times (17 \, k\Omega) = 0.27 \, ms$

The shape of $V_B$ is essentially the same as that of the regular 555 astable configuration, rising and falling exponentially between the two limits - except that the upper limit is $V_R$ instead of $2/3V_{CC}$. Meanwhile $V_A$ rises exponentially from somewhat above $1/3V_{CC}$ to $2/3V_{CC}$, and then drops immediately to zero for the duration of the discharge half-cycle since it is connected directly to the discharge pin (pin 7).